

Characterization of rock material by point load strength index test and direct cut

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Abstract: The objective of this work is to establish a relationship between the cutting time in rocks, determining a speed and the point load strength index test, I_s (50), to characterize the rock in terms of resistance and avoid sending samples to laboratories. As a first stage, on andesite samples, 5 x 5 x 10 cm test tubes were made. After the elaboration they were subjected to cutting, using an electric floor cutter and the time was evaluated. This cut was made in a transversal way and two parts were obtained, one of them with dimensions 5 x 5 x 5 cm, approximately. In a third stage, the point load strength test was carried out in a press built for this purpose. Finally, the cutting speeds were correlated with the point load test values and only when rock samples do not pigeonhole on the proposed relationship, send them to the laboratory.

Keywords: Mining fortification, uniaxial compressive strength, rock cutting, point load strength test index.

Caracterización del material rocoso mediante ensayos de resistencia a carga puntual y corte directo

Resumen: El objetivo de este trabajo es establecer una relación entre el tiempo de corte en rocas, determinando una velocidad y el índice de carga puntual, I_s (50), para caracterizar la roca en términos de resistencia y prescindir del envío de muestras a laboratorios. Como primera etapa, sobre muestras de andesita, se elaboraron probetas de 5 x 5 x 10 cm. Luego de la elaboración se las sometió a corte, mediante una cortadora eléctrica de piso y se evaluó el tiempo. Este corte se realizó de forma transversal y se obtuvieron dos partes, una de ellas con dimensiones 5 x 5 x 5 cm, aproximadamente. En una tercera etapa se ejecutaron los exámenes de carga puntual en una prensa construida para el efecto. Finalmente se correlacionaron las velocidades de corte con los valores de carga puntual y solamente cuando muestras de roca no encasillen sobre la relación propuesta, enviarlas al laboratorio.

Palabras clave: Fortificación minera, resistencia a la compresión uniaxial, corte en rocas, índice de carga puntual.



I. INTRODUCTION

In the development of mining structures, such as slopes and tunnels, which are executed for the extraction of mineral resources or materials intended for construction, it's very important to maintain the strategies for the stability of said structures, therefore, to ensure that they remain firm to avoid landslides and/or collapses in all phases of exploitation of the mining project, managing to generate safety for workers and the equipment.

Achieving the stability of the rocky massifs in the exploitation areas is not an easy task, it initially involves obtaining a series of specific data and parameters, some of which are very difficult to calculate in the field and it is necessary to take of samples or controls (test tubes), which must be sent to laboratories for treatment.

These parameters or data range from visualizations and measurements in the rocky massif itself, to obtaining the resistance to simple or uniaxial compression of the rocky material. There is a clear difference between rocky massif and rocky material, the first concept comprises the outcrop including its discontinuities, joints, or joints, while the rocky material is a compact block of the outcrop.

The resistance to simple compression of the rock material or simply of the rock, is a fundamental parameter that must be included within the estimates in the different geomechanical classifications, such as the RMR or Q Index, but its calculation and determination must be carried out in the laboratory, becoming a tedious and expensive activity in the development of the project. An alternative to the determination of the simple compressive strength of the rock is the so-called point load strength index test or I_s (50), which provides an estimated value of the load on the rock specimen and it is correlated with the simple compressive strength. The I_s (50) test is in situ and inexpensive, which is why it is applied today. Knowing that the rock also presents difficulty in cutting, we try to evaluate its relationship with the I_s (50) test.

In this work it is proposed from the theoretical basis used for the effect, the development of the activities that must be fully followed, the methodology to obtain the resistance to simple compression of the rock through the use of the point load strength index test, the cut of the rock, describing a clear and statistical procedure, which can be used in a mining project, generating a strategy to obtain the parameter with an easy-to-use final mathematical relationship, it should be emphasized that in this work the results obtained have generated a very important expectation about your application.

II. DEVELOPMENT

In this document, we will begin with a description of the concepts and theoretical basis regarding the stability of mining structures, both in open pit and underground. Currently the fundamental problem for Mining Engineers is the need to apply technical tests in situ, but it is essential to know the limitations and properties of the methods in order to establish a solution to the problem. 1.

In Rock Mechanics, which is in charge of studying the properties of rocks and rock masses, it is very important to define some of them, which, without diminishing the importance of others, are considered a priority. The behavior of a mass or massif of rock in situ is different from a rocky material, because the rocky material is much stronger and a rock mass usually presents systems of structural weaknesses called joints, fractures, fissures, discontinuities, faults. Of various sizes 2.

For the development of mining activities, the stability and support of galleries or slopes is a fundamental part and is established as one of the most important tasks, since the correct fortification fulfills its objective of avoiding collapse or falling blocks and consequently, guarantees the safety, mainly of personnel, tools or equipment and production, so that in this way, with adequate and technical fortification, it will be possible to avoid work accidents. Therefore, we can generate, for the staff, a safe area and work environment, achieving greater performance and providing security for the company. 3. This need has led to the development of so-called geomechanical classifications, which use a series of parameters for the evaluation of rock masses.

Nowadays, geomechanical classifications have become widespread and are widely used, both in the design and execution phases, in all types of works in rock massifs. It is therefore important to know the limitations and difficulties that each of the classifications presents. 4 and a fundamental parameter is the resistance to simple compression or point load strength index test, I_s (50). However, many times due to the conditions in which the mining works are found, it's complicated and sometimes almost impossible to send rock samples to laboratories to determine the value of the UCS, and in these times, it is the problem of those in charge of evaluating stability. Of the structures in the field, which is why, there is an urgent need to generate alternatives in situ for the assessment

of the UCS 5. Therefore, the necessary bases for the development of the proposal are specified below.

Rocks are natural aggregates of mineral particles; they combine through a strong permanent cohesion. If its resistance to simple compression (without drainage) is greater than 5 kg/cm², it's generally considered a rock 6.

The rocks that make up the earth's crust are divided into three categories: igneous rocks, metamorphic rocks, and sedimentary rocks. Igneous rocks are formed by cooling and solidifying agglomerates of hot fluid called magma. The chemical composition of the first 16 Km of the crust clearly shows that some elements such as Si, O, Fe and Al dominate and account for approximately 87%. Followed by the alkaline earth and alkaline ones: Ca, Mg, Na and K. In a small proportion, Ti, P, Mn, S, Cl and C 7.

The foundations of this work begin with obtaining samples of the rock studied comes from an outcrop located in the province of Cañar (Ecuador), in the sector called Cojitambo, an outcrop composed of a travertine and a volcanic formation of the andesite type 8. Andesites are fine-grained volcanic rocks, they are common, as lava flows in orogenic regions and occasionally form small intrusions. They are compact, sometimes vesicular and commonly brown in color, and in total extent, they rank second after basalt. Many andesite flows are found in continental areas in the Andes of South America (from which they take their name) where many volcanoes have emitted ash and lava of andesitic composition 9. If this is the case, the phenocrysts are generally transparent rectangular plagioclase crystals or elongated black amphibole crystals. Andesite contains small amounts of quartz, while rhyolite consists of approximately 25 percent quartz 10.

A. Rock cutting

Rock cutting is an activity in which the skill and experience of the operator predominates, however, having the appropriate machinery it can be developed without inconvenience by a worker.

One of the properties to consider when cutting rocks is the versatility of the cutting machine, particularly with regard to the possibility of varying the performance and peripheral speed of the blade during the cutting process. 11. We should consider that cutting a material requires the power consumption of the saw, so that for hard materials and high cutting conditions, the cutting speed or the cutting rate is required as the cut rock surface. In these cases, if we are keeping the cutting rate, the peripheral speed of the blade can increase, reducing energy consumption.

Initial considerations should be taken into account when choosing cutting equipment, it's done based on detecting the following intrinsic aspects of the rock such as abrasiveness, compressive strength, toughness, hardness, porosity, etc. It is also necessary to take into account the rate of production and the degree of mechanization of the tasks to be done. 2.

The Covington's disc cutting machine consists of a tile saw and is a high-performance floor model for cutting glass and stone. This is a plunge saw, meaning the cutting fluid is deposited into the tank and the rotating saw blade lifts the cutting fluid up and around the part. Covington lines the saw tank, hood, and chassis for durability and longevity. The hood fits exactly into the tank and prevents leaks. The hood can be opened with a sturdy steel arm for easy loading and unloading of parts 13.

B. Unconfined Compressive Strength

The unconfined compressive strength of rocks is the most common measure to define the reasons for failure and the geomechanical procedure of a given rock mass. To obtain it in the laboratory examinations, it requires scrupulously prepared samples and a certain considerable time to be able to know the result, which can present a high cost. Anisotropic rocks in particular are difficult to perform tests due to their variant resistance, so numerous laboratory tests are necessary to obtain representative parameters of the entire resistance range 14. The resistance of a rock is the result of the stress that it undergoes when it breaks. When the resistance is calculated in unconfined rock specimens, it is designated simple compression resistance and its value is used for the geotechnical classification of rocks. To obtain this property, the simple compression test is used.

The purpose of this test is to measure the compressive strength of a rock specimen, subjected to an axial load. To carry out the test, it is necessary to have a press of adequate capacity that allows to use the load on the specimen at a constant speed until it breaks in a time interval between 5 and 15 minutes, also the loading speed can be set between intervals of 0.5 to 1 MPa/s 15. The specimen is placed between the discs of the press, well centered. Where a settlement load equivalent to 1% of the estimated simple compressive strength is applied. At this time, the charge indicator clock is reset. The speed of application of the load is fixed, beginning the compression, until the sample breaks.

Equation (1) shows us how to determine the simple compressive strength of a specimen:

$$UCS = \sigma_c = \frac{P}{A} \quad (1)$$

Where:

P = is the maximum load to which the specimen has been subjected during the test.

A = is the cross-sectional area of the specimen.

C. The Point Load Strength Index Test

The point load strength index test is one of the most important tests used for the indirect determination of UCS, since in the implementation of the press it can be used in situ or in a laboratory, in addition to that requires little or no sample preparation for testing 16. The point load or break test between points is a basic test that can be carried out in the field with cores without modification or with rock fragments. This is based on applying a point load to a piece of rock until it breaks, obtaining an Is index that is correlated with the simple compressive strength of the rock. 17. The point load strength index test value can be used as an indirect estimate of the uniaxial or simple compression of the rock, the sample that is carried out may be a rock core, a block or an irregular rock lump 18.

The point load test consists of breaking a piece of rock between two conical points of hardened steel. The samples that will later be placed between said tips can be of any shape, but it is recommended that their diameter is not less than 50 mm, since the volume of said test piece influences its resistance.

Equation 2 allows us to calculate the point load index without correction:

$$I_s = \frac{P}{(De)^2} \quad (2)$$

Where:

P = applied load in N.

De = equivalent core diameter in mm 19.

The distances of the fragments are taken which must obey with the provisions indicated in the standard. The ratio $0.3 < D / W < 1$ is preferably close to 1. The distance $L > 0.5W$ (L distance from the end of the rock to the conical points) and the W.

Equation 3 determines the equivalent diameter De as a function of the dimensions of the irregular fragments:

$$(De)^2 = \frac{4A}{\pi} \quad (3)$$

Where:

$$A = WD \quad (4)$$

Where A is the minimum cross-sectional area parallel to the direction of the load in mm².

The corrected point load strength index test, Is (50) of a rock sample is defined as the value of Is that has been measured by a diametral test with D = 50 mm. When a rock classification is essential, the most reliable method to achieve Is (50) is to carry out the tests with diameters of D = 50 mm or very close to this value. Most point load tests are carried out using sample sizes other than the mentioned diameter 20.

In equation 5 we can obtain the size correction:

$$I_s(50) = \left(\frac{De}{50}\right)^{0.45} \cdot I_s \quad (5)$$

Finally, in equation 6 we can observe the relationship between the resistance to simple compression of the rock specimen, related to the point load index 21.

$$I_s = \frac{\sigma_c}{14 + 0.175D} \quad (6)$$

III.METHODOLOGY

At this point, it will be presented to you a detailed explanation of the operations carried out to achieve the objectives established in this work. We will start with a description of the number of samples with their respective preparation, their cutting process, the execution of the point load strength index test and the determination of the simple compressive strength.

Initially, 60 samples were taken from the study area, which is located in the sector called Cojitambo, in the province of Cañar (Ecuador), this can be seen in the figure 1.



Fig. 1. Cojitambo

Subsequently, cuttings were carried out on each of the samples to obtain specimens of approximately 5x5x10 cm. Once the specimens are created, it is verified that they do not have cracks and that the dimensions are very close to those mentioned above. A specimen ready for cutting can be seen in figure 2, and another specimen after cutting in figure 3.



Fig. 2. Rock specimen ready for cutting



Fig. 3. Rock specimen after cutting

Before starting the cutting process, the distances that exist between the jaw and the disk must be measured in conjunction with the specimen and draw a line on the specimen to be able to make the appropriate cut that is needed, as shown in the figure 2.



Fig. 4. Covington Floor Saw

It's necessary to emphasize that the cutter used was a floor Covington and it was worked with a 30 cm disc radius and with 78.14 liters of water-oil. The fluid must always be in a 10: 1 ratio. The cutter can be seen in figure 4.

The selected specimen passes to the cutting process in which the time of its execution carried out by the disc cutter is taken, resulting in two specimens of different dimensions, the first with measurements of approximately 5x5x5 cm that will later be used to execute the point load rupture and the second specimen with approximate dimensions 5x5x4.3 cm will be used for the rupture in simple compression. It is important at this point to establish that the cutting time is evaluated in each specimen with the premise that, if the specimen presents greater resistance, the cutting time will be longer or if the specimen is less hard, the time will be shorter, this due to the anisotropy of the rocks. It is also necessary to clarify that the dimensions of the initial 5x5x10 cm specimens are established so that when cutting, two elements are produced that obtain the dimensions and relationships necessary by the standard, both for the point load index test, and for determination of compressive strength.

Once the described specimens are obtained, the point loading process begins, in a press built for this purpose, the press can be seen in figure 5.



Fig. 5. Point load strength index test Press

As a final step, the specimens for compressive strength are taken and subjected to the respective test, the Humboldt machine used for this test can be seen in Figure 6.

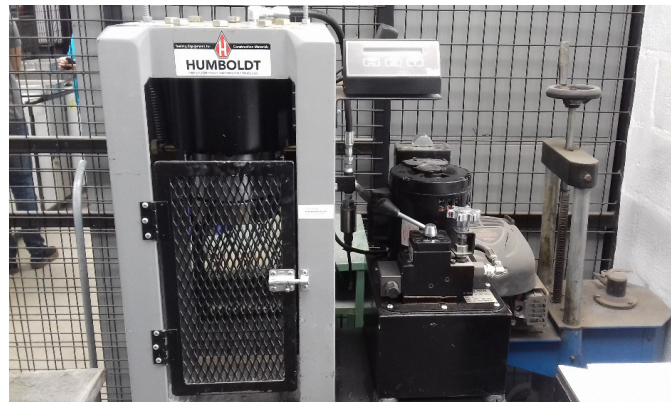


Fig. 6. Humboldt resistance press

IV.RESULTS

After executing all the tests, it has been possible to obtain a series of data which in their treatment will represent different relationships between the parameters obtained. Initially, Table 1 is shown, in which the results of cutting time and cutting speed are presented.

Table 1. Results of the cutting speed.

Test tube	speed (mm/min)	Test tube	speed (mm/min)	Test tube	speed (mm/min)	Test tube	speed (mm/min)
1	1.951	16	2.056	31	2.087	46	2.121
2	1.978	17	2.057	32	2.087	47	2.130
3	1.986	18	2.058	33	2.091	48	2.131
4	2.011	19	2.058	34	2.091	49	2.133
5	2.016	20	2.060	35	2.092	50	2.141
6	2.017	21	2.064	36	2.098	51	2.142
7	2.018	22	2.064	37	2.101	52	2.145
8	2.030	23	2.065	38	2.105	53	2.150
9	2.035	24	2.065	39	2.106	54	2.151
10	2.038	25	2.069	40	2.108	55	2.164
11	2.039	26	2.070	41	2.109	56	2.173
12	2.040	27	2.072	42	2.116	57	2.178
13	2.045	28	2.078	43	2.117	58	2.184
14	2.051	29	2.082	44	2.118	59	2.185
15	2.055	30	2.084	45	2.120	60	2.193

Table 2. Results of the point load strength index test by test in a conical point press

Test tube	Is (MPa)	Test tube	Is (MPa)	Test tube	Is (MPa)	Test tube	Is (MPa)
1	2.412	16	2.926	31	3.069	46	3.183
2	2.451	17	2.938	32	3.069	47	3.196
3	2.474	18	2.939	33	3.099	48	3.213
4	2.699	19	2.939	34	3.101	49	3.216
5	2.756	20	2.939	35	3.101	50	3.216
6	2.756	21	2.955	36	3.115	51	3.261
7	2.816	22	2.972	37	3.119	52	3.279
8	2.842	23	2.986	38	3.131	53	3.315
9	2.842	24	3.005	39	3.165	54	3.324
10	2.842	25	3.035	40	3.165	55	3.329
11	2.881	26	3.036	41	3.181	56	3.330
12	2.894	27	3.036	42	3.183	57	3.410
13	2.896	28	3.052	43	3.183	58	3.450
14	2.908	29	3.052	44	3.183	59	3.524
15	2.910	30	3.069	45	3.183	60	3.635

Finally, in table 3 we can see the results of the compressive strength tests of the specimens.

Table 3. Results of the point load strength index test by test in the Humboldt press

Test tube	Is (MPa)	Test tube	Is (MPa)	Test tube	Is (MPa)	Test tube	Is (MPa)
1	1.106	16	1.441	31	1.640	46	1.855
2	1.136	17	1.458	32	1.653	47	1.874
3	1.181	18	1.475	33	1.658	48	1.894
4	1.210	19	1.489	34	1.664	49	1.905
5	1.217	20	1.493	35	1.669	50	1.916
6	1.261	21	1.523	36	1.711	51	1.931
7	1.355	22	1.542	37	1.729	52	1.972
8	1.368	23	1.605	38	1.762	53	1.973
9	1.380	24	1.609	39	1.762	54	1.992
10	1.385	25	1.614	40	1.776	55	2.126
11	1.409	26	1.619	41	1.784	56	2.183
12	1.410	27	1.624	42	1.787	57	2.209
13	1.413	28	1.629	43	1.807	58	2.250
14	1.427	29	1.634	44	1.821	59	2.338
15	1.435	30	1.637	45	1.840	60	2.377

After analyzing the data, by a reasoning effect, it can be stated that the cutting time is greater when the rock resistance is greater, consequently, the cutting speed the lower it is, and the compressive strength of the specimen is greater.

This statement leads us to generate, both for the point load strength index test in the conical tip press, and for the point load index due to the resistance to simple compression, the following graphs (Figures 7 and 8).

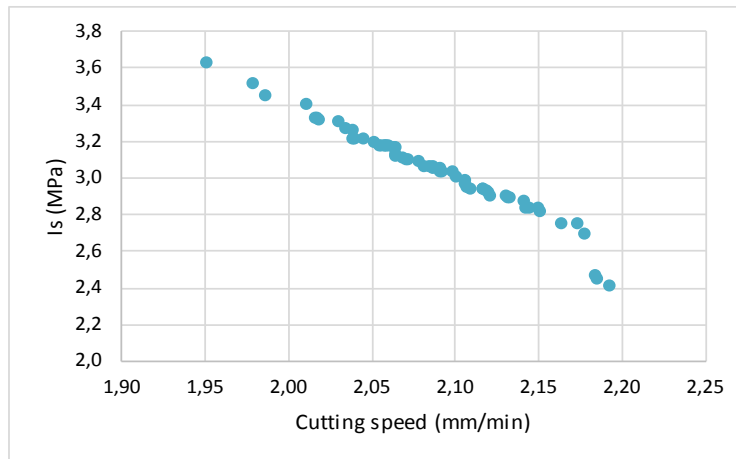


Fig. 7. Results of the Point load index in conical tips vs. Cutting speed

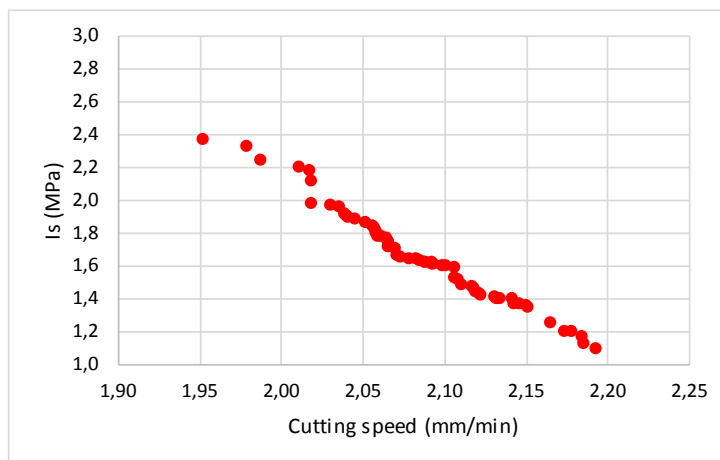


Fig. 8. Humboldt Press Point Load Index Results Graph vs. Cutting speed

Having seen the graphics and adding the respective trend lines, which have the highest R², the following equations are proposed, (7) for the point load index obtained in the conical point press and (8) for the point load index obtained from the Humboldt press:

$$I_s = -4.3544 \cdot Vc + 12.138 \quad (7)$$

$$R^2 = 0.9603$$

$$I_s = -5.4836 \cdot Vc + 13.107 \quad (8)$$

$$R^2 = 0.9789$$

By observing the equations, we can indicate that in practical terms they both have the same slope and we can execute a final correction. For a better observation of the graphs, Figure 9 is presented.

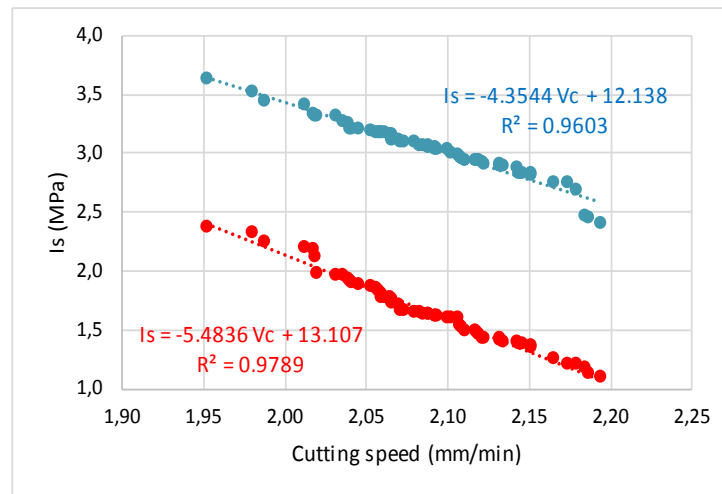


Fig. 9. Equations and trend lines of processes

If a speed, for this same type of rocky material, is 2 mm/min, the point load strength index test generates a value of 3.4292 MPa, while, with the equation for simple compressive strength, the point load strength index test it is 2.1398 MPa, which we must correct towards the final value. When comparing the equations, we can state that between the two there is an error that could be reduced considerably if the equation is proposed:

$$I_s = -4.919 \cdot Vc + 11.838 \quad (9)$$

Which has been obtained with the mean of the slopes and subtracting 0.3 from the intercept value of the line. With equation (9) it is determined that the error is approximately 6.5%, which for classification purposes of the rock type is quite acceptable.

V. CONCLUSIONS

With this research, an alternative is proposed to obtain the resistance to simple compression of rocks, through the point load index, in mining operations, in order to solve the problem of sending samples to the laboratory, generating savings in time and money.

The correlations obtained between the cutting speed and the point load index, I_s (50), as well as with the resistance to simple compression, are acceptable due to the fact that they present an R^2 with values between 0.9 to 1.

Since the study was carried out in the Cojitambo area and there are optimal results of the resistance of the andesite rock, the use of this research for the exploitation of said material is very favorable, since said rock is used for driveways, paths, curbs, decorative coatings for homes, buildings and roads, because their point load index ranges from 1.1 to 2.4 MPa.

The equipment used in this research is appropriate and suitable for each of the processes carried out, for this reason optimal results have been achieved that have guaranteed our alternative as an excellent option to find the point load strength index test, I_s (50), for the aforementioned are feasible for such equipment to be acquired in a mining camp.

With this research and the proposed methodology, it can be generalized and carried out in a mining project, with reliable results, but because it is perfectible, more case studies can be generated, modifying the different variables present in the study.

REFERENCES

[1] P. Feijoo, R. Aucay, D. Ordoñez, "Aplicación del esclerómetro para la determinación de resistencia a compresión de rocas", presentado en el IV Congreso Internacional de Minería y Metalurgia (MINEMETAL), Varadero,

Cuba, 2018.

[2]P. Feijoo y M. Román, «Correlación entre la Deformación y la Resistencia a la Compresión de rocas», uct, vol. 23, n.º 91, p. 6, may. 2019.

[3]P. Feijoo, A. Bravo, N. Escandón, "Aplicación "UDAFORMIN" para la determinación del tipo de fortificación minera", presentado en el XII Congreso Iberoamericano de Computación para el Desarrollo (COMPDES), San Salvador, El Salvador, 2019.

[4]P. Feijoo y C. Iñiguez, «Corte en las Rocas y su Relación con la Resistencia a Compresión Simple», RISTI, n.º E 30, p. 59-67, jun. 2020.

[5]P. Feijoo y J. Padrón, «La Resistividad de Rocas y su Relación con la Resistencia a Compresión Simple en Mina», UCT, vol. 24, n.º 99, pp. 61-67, abr. 2020.

[6]M. González. El terreno. Ediciones UPC. Barcelona. España, 2001.

[7]E. Besoain. Mineralogía de Suelos. Turrialba: Instituto Interamericano de Ciencias Agrícolas de la OEA, 1970.

[8]P. Feijoo, A. Flores, B. Feijoo, "The Concept of the Granulometric Area and Its Relation with the Resistance to the Simple Compression of Rocks", presentado en la 7th International Engineering, Sciences and Technology Conference (IESTEC), Panamá, Panamá, 2019, pp. 52-56, doi: 10.1109/IESTEC46403.2019.00018

[9]F. Blyth. Geología para Ingenieros. Cecsca. México D. F. México, 2003.

[10] E. Tarbuck & F. Lutgens. Ciencias de la Tierra: Una introducción a la Geología Física. Pearson. Madrid. España, 2005.

[11]L. Suarez del Rio, A. Rodríguez, L. Calleja, V. Ruiz de Argandoña, «El corte de rocas ornamentales con discos diamantados: influencia de los factores propios del sistema de corte», CSIC, vol. 48, n.º 250, pp. 53-59, abr-may-jun 1998.

[12]Universidad Politécnica de Madrid. Explotaciones de Roca Ornamental. Diseño de explotaciones y selección de maquinaria y equipos. UPM. Madrid. España, 2007.

[13]Catalog, Covington, (2019). LAPIDARY & GLASS MACHINERY, USA. Retrieved from <https://covington-engineering.com/content/pdf/Covington-Catalog.pdf>

[14]D. Burbano, T. García, «Estimación empírica de la resistencia a compresión simple a partir del ensayo de carga puntual en rocas anisótropas (esquistos y pizarras)», FIGEMPA, vol.1, n.º 2, pp. 13-16, dic. 2016.

[15]P. Ramírez, L. de la Cuadra, R. Lain, E. Grigalbo. Mecánica de rocas aplicada a la minería metálica subterránea. Instituto Geológico Minero. Madrid. España, 1984.

[16]P. Cordero, "Manual de prácticas de laboratorio de Mecánica de Rocas (Parte I)" tesis, Universidad Nacional Autónoma de México, México D.F., México, 2019.

[17]L. González de Vallejo, M. Ferrer. Manual de campo para la descripción y caracterización de macizos rocosos en afloramientos. Instituto Geológico y Minero de España. Madrid. España, 2007.

[18]P. Pohjanpera, T. Wanne, E., Johansson. Point Load Test Results From Olkiluoto Area Borehole Cores. Posiva. Finlandia, 2005.

[19]P. Ramírez, L. Alejano. Mecánica de rocas: fundamentos e ingeniería de taludes. Universidad Politécnica de Madrid. Madrid. España, 2004.

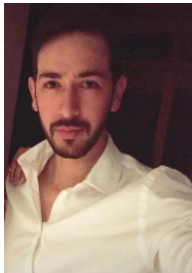
[20]M. Navarrete, W. Martínez, E. Alonso, C. Lara, A. Bedolla, H. Chávez, D. Delgado, J. Arteaga. «Caracterización de propiedades físico-mecánicas de rocas ígneas utilizadas en obras de infraestructura», ALCONPANT, vol. 3, n.º 2, pp. 133-143, ago. 2013.

[21]P. Feijoo, "Manual de mecánica de rocas y estabilidad de túneles y taludes" tesis, Universidad del Azuay, Cuenca, Ecuador, 1997.

RESUMEN CURRICULAR



Patricio Feijoo, Mining Engineer, graduated from the University of Azuay (Cuenca-Ecuador), with studies and internships in: Bolivia, Brazil, Spain, Australia in areas of geology, geophysics and development of mining activities. He is linked to teaching at the University of Azuay.



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